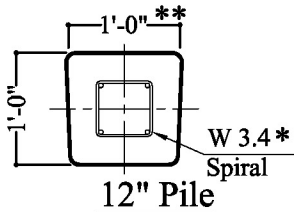




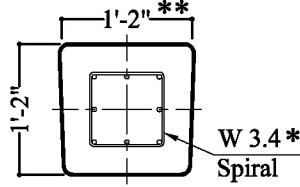
Standard

CONCRETE PRODUCTS



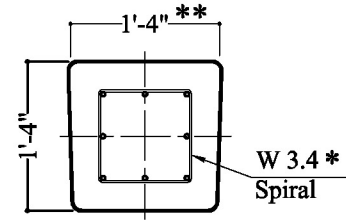
12" Pile

Strand Pattern (typ.) - 4 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270 LRS, at 31 kips
A=144 in²;
Ix-x=1728 in⁴;
Yb=6.00 in;
Wt=150 plf



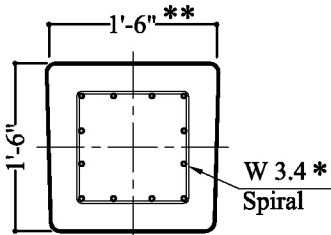
14" Pile

Strand Pattern (typ.) - 8 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270 LRS, at 31.0 kips
A=196 in²;
Ix-x=3201 in⁴;
Yb=7.00 in;
Wt=204 plf



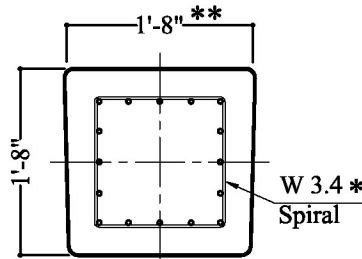
16" Pile

Strand Pattern (typ.) - 8 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270 (Spec.) LRS, at 34.0 kips
A=256 in²;
Ix-x=5461 in⁴;
Yb=8.00 in;
Wt=267 plf



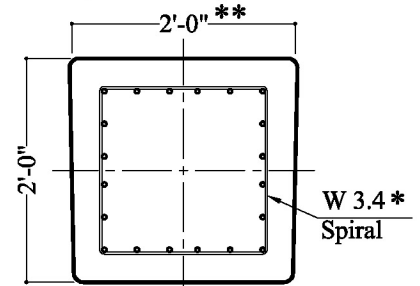
18" Pile

Strand Pattern (typ.) - 12 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270 (Spec.) LRS, at 34.0 kips
A=324 in²;
Ix-x=8748 in⁴;
Yb=9.00 in;
Wt=338 plf



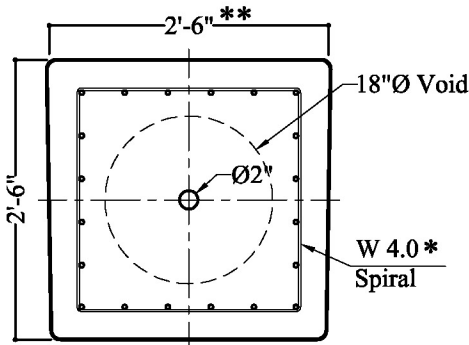
20" Pile

Strand Pattern (typ.) - 16 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270 LRS, at 31.0 kips
A=400 in²;
Ix-x=13,333 in⁴;
Yb=10.00 in;
Wt=417 plf



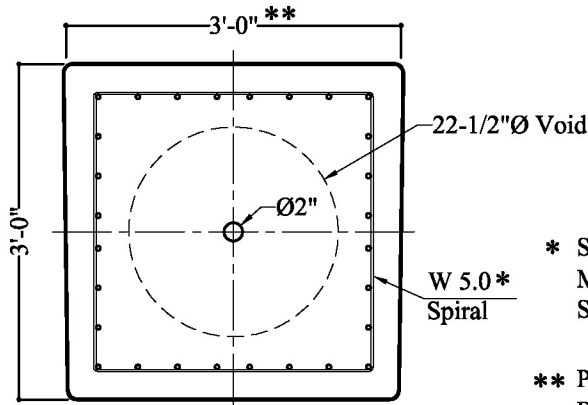
24" Pile

Strand Pattern (typ.) - 20 ~ $\frac{1}{2}$ " $\varnothing$,
Grade 270(spec.)LRS, at 34.0 kips
A=576 in²;
Ix-x=27,648 in⁴;
Yb=12.00 in;
Wt=600 plf



30" Pile

Strand Pattern (typ.) - 20 ~ 0.6" $\varnothing$,
Grade 270 LRS, at 41.0 kips
A=900 in²;
Ix-x=67,500 in⁴;
Yb=15.00 in;
Wt=683 plf - Voided Section



36" Pile

Strand Pattern - Varies per Project
A=1,296 in²;
Ix-x=139,968 in⁴;
Yb=18 in;
Wt= 953 plf - Voided Section

* SPIRAL & STRAND PATTERN
MAY CHANGE FROM
STATE TO STATE.

** PILE FORMS HAVE A 3/8" MIN.
DRAFT TO ALLOW FORM REMOVAL
DIMENSION IS FROM CENTER OF PILE

ALL PILE CORNERS ARE
ROUNDED UP TO 1" RADIUS.
ALL WEIGHTS ARE NOMINAL.

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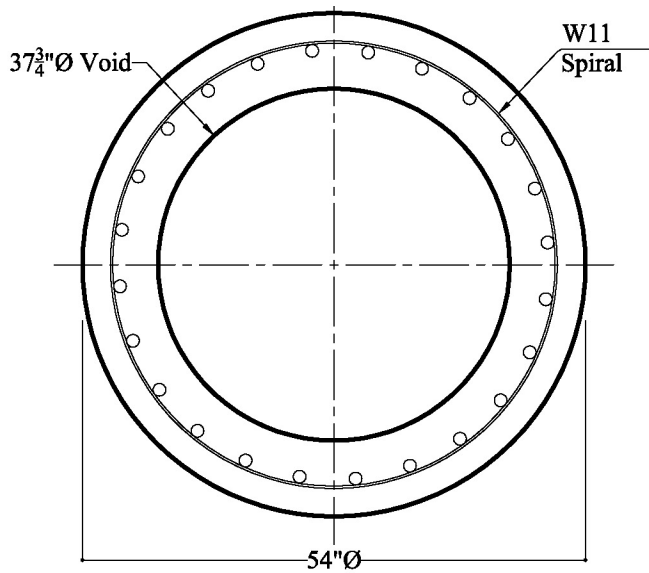
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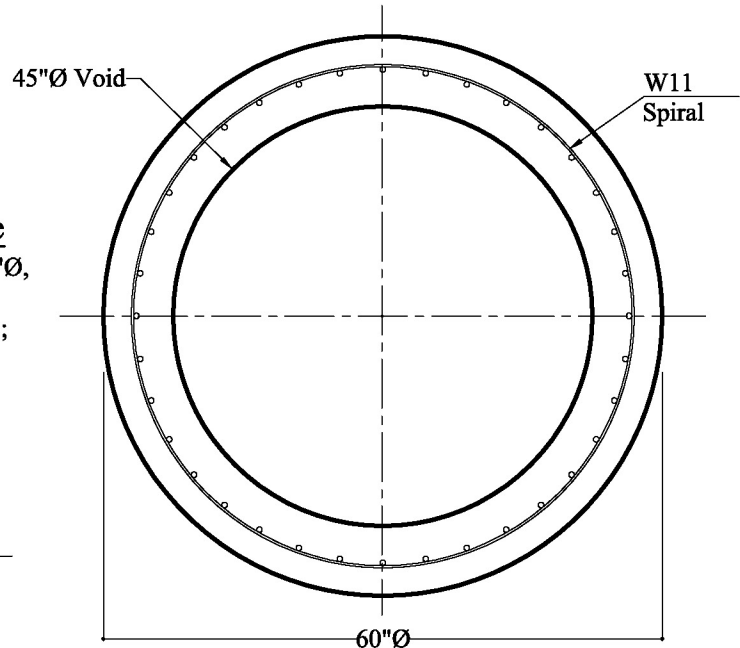


54" Cylinder Pile

Strand Pattern - $\frac{1}{2}$ " $\emptyset$ (Spec.),
Qty.=48(2 strands per Tendon)
 $A=1,171 \text{ in}^2$;
 $I_x-x=I_y-y=317,706 \text{ in}^4$;
 $Y_b=Y_t=27.00 \text{ in}$;
 $Z_b=Z_t=11,767 \text{ in}^3$;
 $W_t=1,220 \text{ plf}$

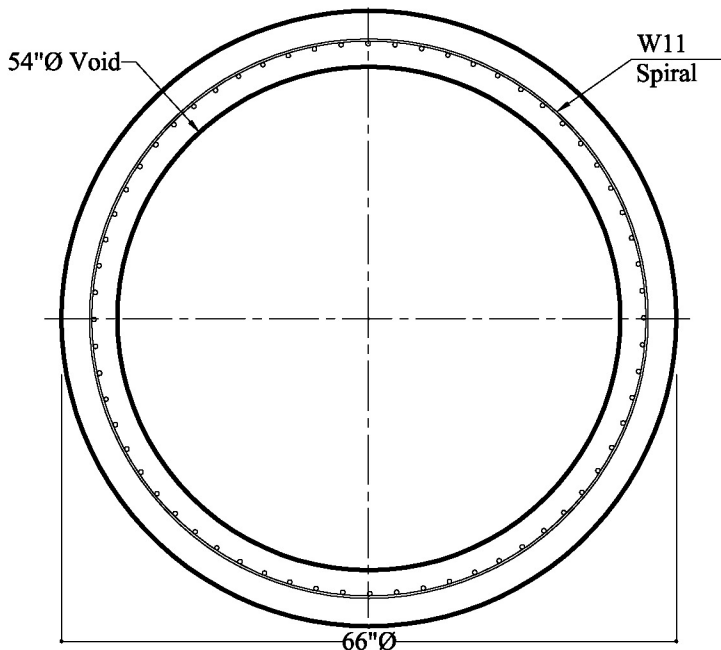
60" Cylinder Pile

Strand Pattern - 36 ~ 0.6" $\emptyset$,
 $A=1,237 \text{ in}^2$;
 $I_x-x=I_y-y=434,883.5 \text{ in}^4$;
 $Y_b=Y_t=30.00 \text{ in}$;
 $Z_b=Z_t=14,496 \text{ in}^3$;
 $W_t=1288.5 \text{ plf}$



66" Cylinder Pile

Strand Pattern - 64 ~ .5" $\emptyset$,
 $A=1,131 \text{ in}^2$;
 $I_x-x=I_y-y=514,027.4 \text{ in}^4$;
 $Y_b=Y_t=33.00 \text{ in}$;
 $Z_b=Z_t=15,577 \text{ in}^3$;
 $W_t=1178 \text{ plf}$



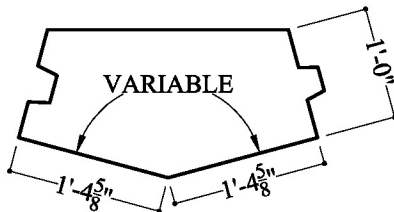
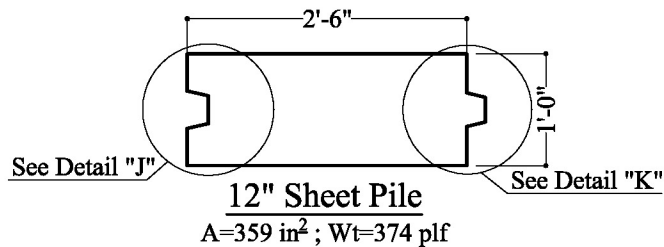
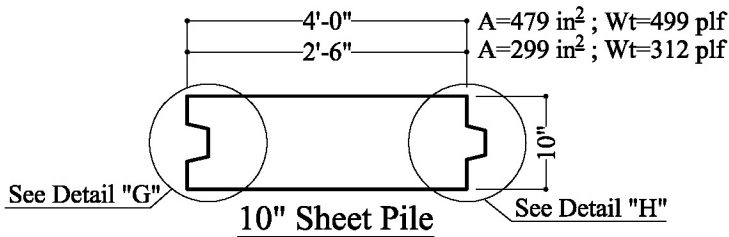
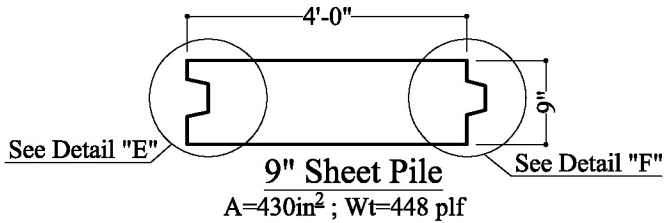
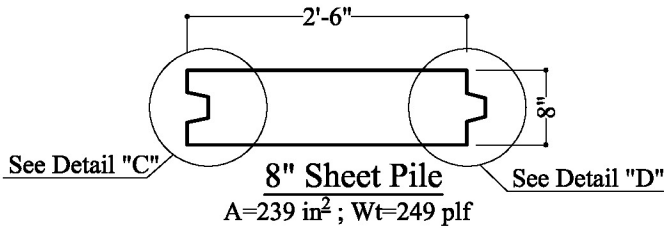
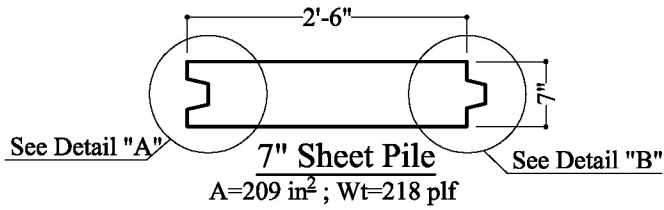
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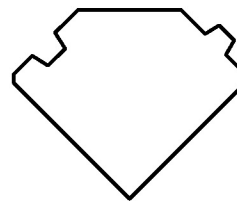
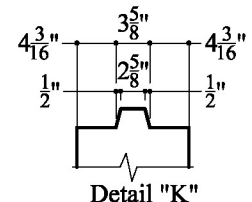
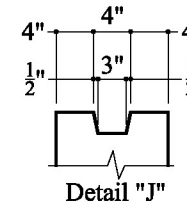
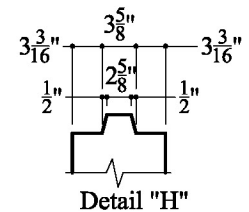
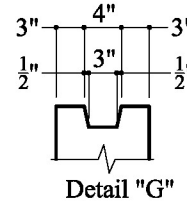
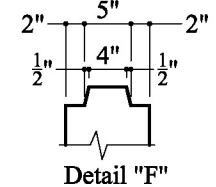
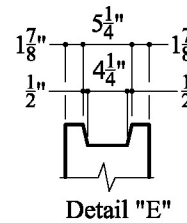
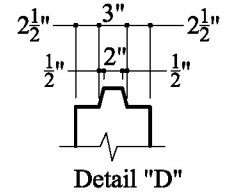
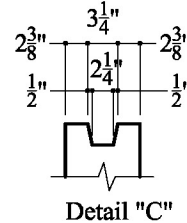
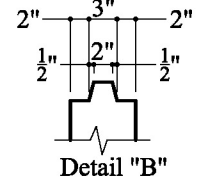
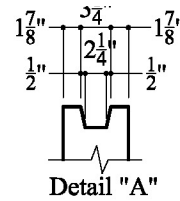
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**Variable Angle
Corner Pile**



**Right Angle
Corner Pile**

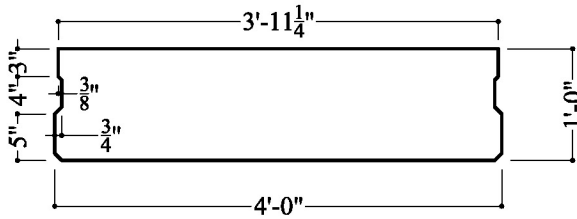
7" & 9" SHEET PILE ARE
TYPICALLY USED IN GA & SC.
ADDITIONAL SIZES
AVAILABLE UPON REQUEST.
ALL WEIGHTS ARE NOMINAL.

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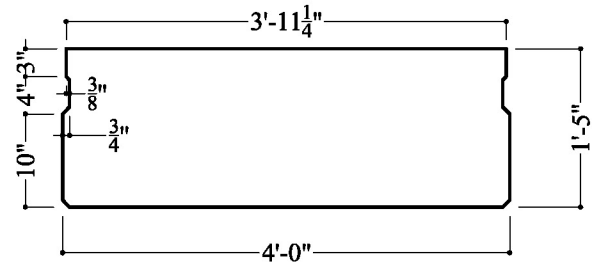
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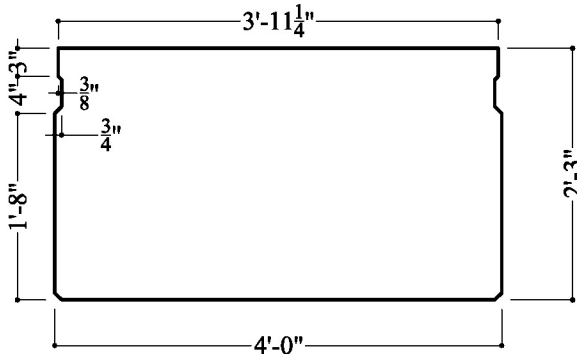
12" x 48" Box Beam

A=808 in² ;
I_{x-x}=19,463 in⁴ ;
Y_b=8.46 in ;
W_t=842 plf



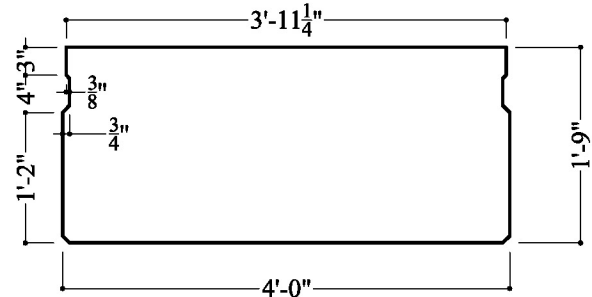
17" x 48" Box Beam

A=808 in² ;
I_{x-x}=19,463 in⁴ ;
Y_b=8.46 in ;
W_t=842 plf



27" x 48" Box Beam

A=1,288 in² ;
I_{x-x}=78,001 in⁴ ;
Y_b=13.44 in ;
W_t=1342 plf

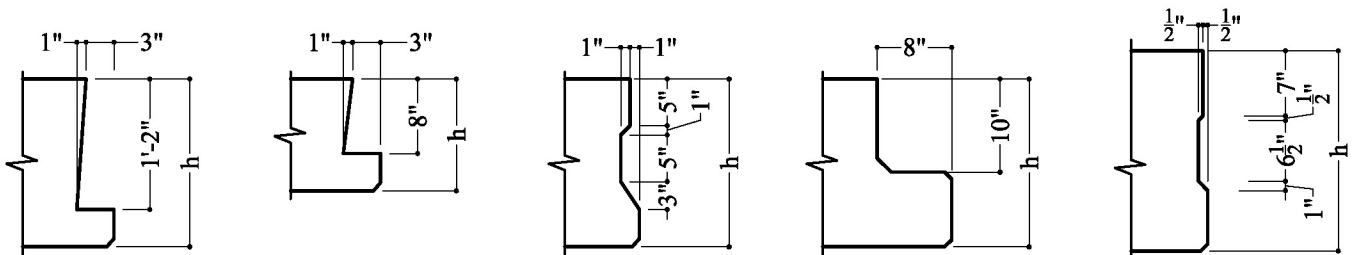


21" x 48" Box Beam

A=1,000 in² ;
I_{x-x}=36,684 in⁴ ;
Y_b=10.45 in ;
W_t=1042 plf

SECTION CAN BE SOLID OR VOIDED .
WIDTH OF PRODUCT MAY VARY FROM 3'-0" to 7'-0".
THICKNESS (DIM "h") OF PRODUCT MAY VARY FROM 10" to 36".
ALL WEIGHTS ARE NOMINAL.

KEYWAY VARIATION OF DECK SLABS & BOX BEAMS



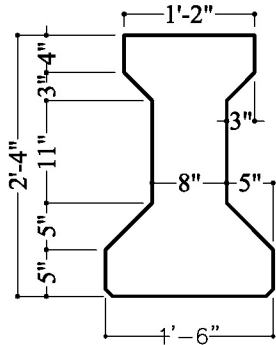
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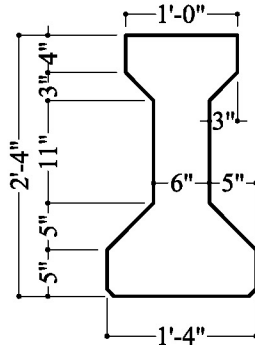
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Family of AASHTO Beams



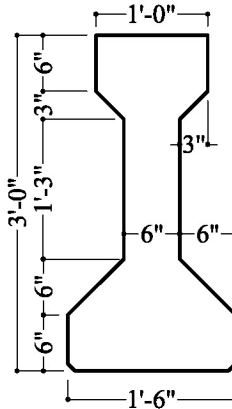
Mod. I Beam

$A=332 \text{ in}^2$
 $I_x-x=26,495 \text{ in}^4$
 $I_y-y=5,222 \text{ in}^4$
 $Y_b=12.83 \text{ in}$
 $W_t=346 \text{ plf}$



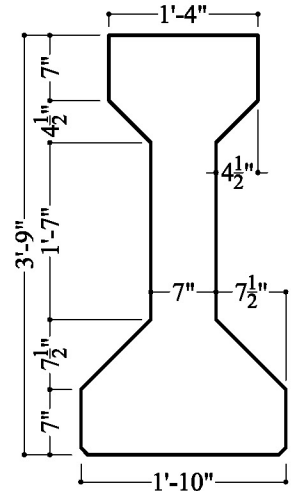
Type I Beam

$A=276 \text{ in}^2$
 $I_x-x=22,744 \text{ in}^4$
 $I_y-y=3,352 \text{ in}^4$
 $Y_b=12.59 \text{ in}$
 $W_t=288 \text{ plf}$



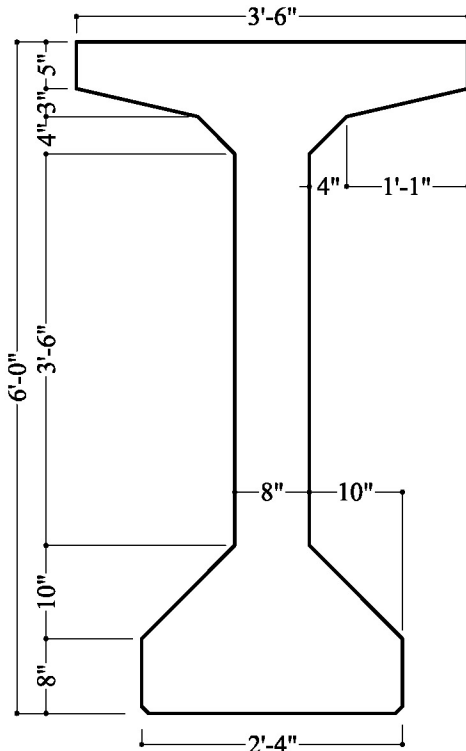
Type II Beam

$A=369 \text{ in}^2$
 $I_x-x=50,979 \text{ in}^4$
 $I_y-y=5,333 \text{ in}^4$
 $Y_b=15.83 \text{ in}$
 $W_t=384 \text{ plf}$



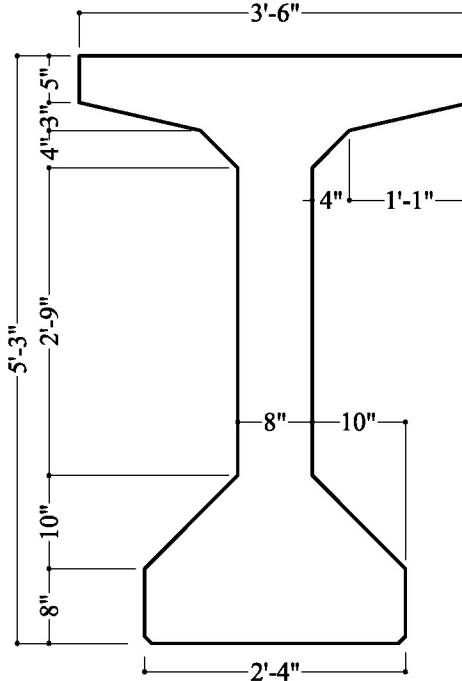
Type III Beam

$A=559 \text{ in}^2$
 $I_x-x=125,390 \text{ in}^4$
 $I_y-y=12,217 \text{ in}^4$
 $Y_b=20.27 \text{ in}$
 $W_t=583 \text{ plf}$



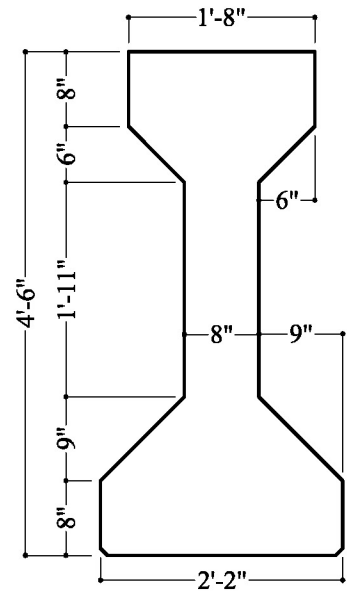
Type VI Beam

$A=1085 \text{ in}^2$
 $I_x-x=732,586 \text{ in}^4$
 $I_y-y=61,513 \text{ in}^4$
 $Y_b=36.39 \text{ in}$
 $W_t=1130 \text{ plf}$



Type V Beam

$A=1,013 \text{ in}^2$
 $I_x-x=520,597 \text{ in}^4$
 $I_y-y=61,129 \text{ in}^4$
 $Y_b=31.96 \text{ in}$
 $W_t=1,055 \text{ plf}$



Type IV Beam

$A=789 \text{ in}^2$
 $I_x-x=260,741 \text{ in}^4$
 $I_y-y=24,374 \text{ in}^4$
 $Y_b=24.73 \text{ in}$
 $W_t=822 \text{ plf}$

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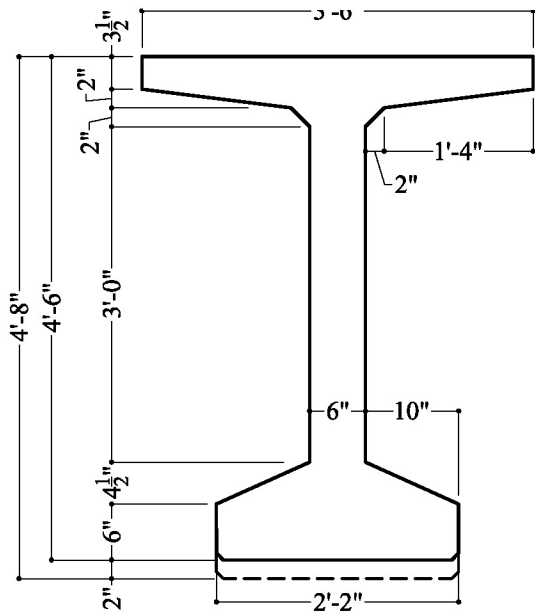
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Standard
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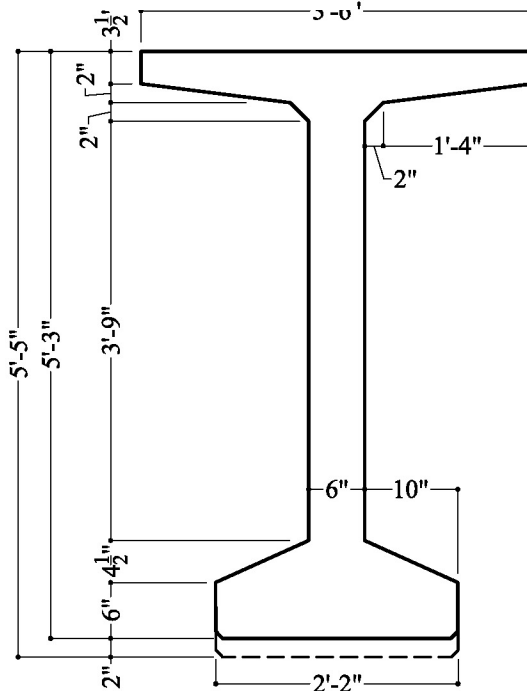
PCI-BT-54

A=659 in²
I_{x-x}=268,051 in⁴
I_{y-y}=37,310 in⁴
Y_b=27.63 in
W_t=686 plf

BT-56

(shown in dashed line)

A=711 in²
I_{x-x}=307,166 in⁴
I_{y-y}=40,148 in⁴
Y_b=27.56 in
W_t=740 plf



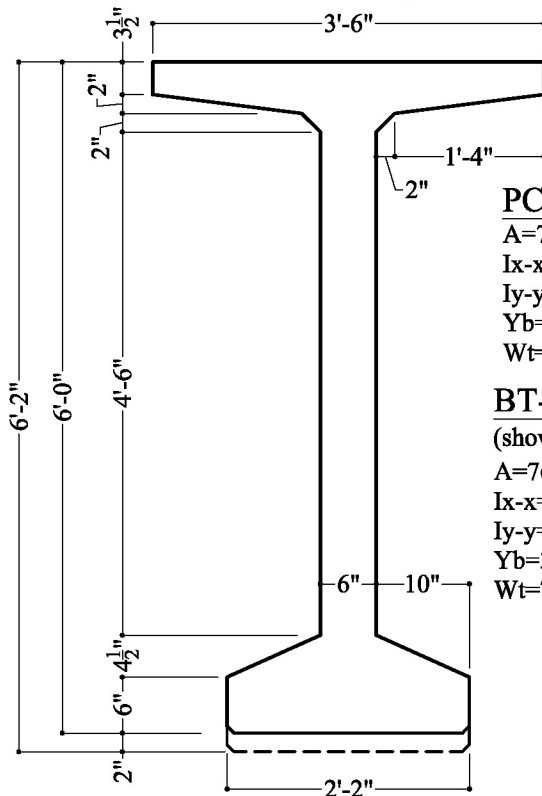
PCI-BT-63

A=713 in²;
I_{x-x}=392,509 in⁴
I_{y-y}=37,472 in⁴
Y_b=32.12 in
W_t=743 plf

BT-65

(shown in dashed line)

A=765 in²;
I_{x-x}=445,127 in⁴
I_{y-y}=40,310 in⁴
Y_b=31.89 in
W_t=796 plf



PCI-BT-72

A=766 in²
I_{x-x}=545,113 in⁴
I_{y-y}=37,543 in⁴
Y_b=36.63 in
W_t=799 plf

BT-74

(shown in dashed line)

A=766 in²
I_{x-x}=545,113 in⁴
I_{y-y}=37,543 in⁴
Y_b=36.63 in
W_t=799 plf

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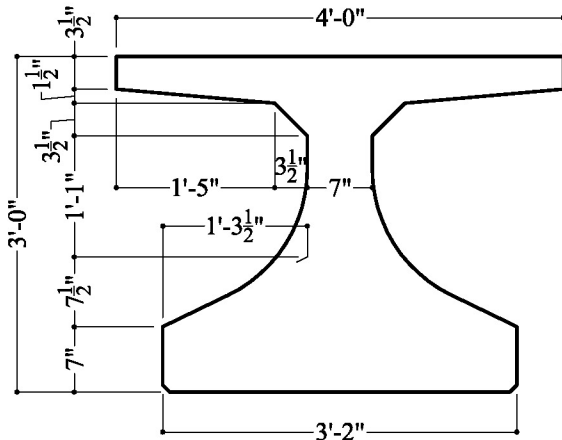
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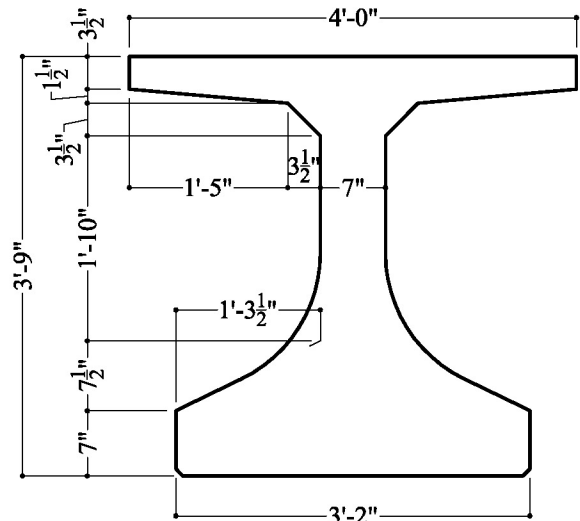


Standard
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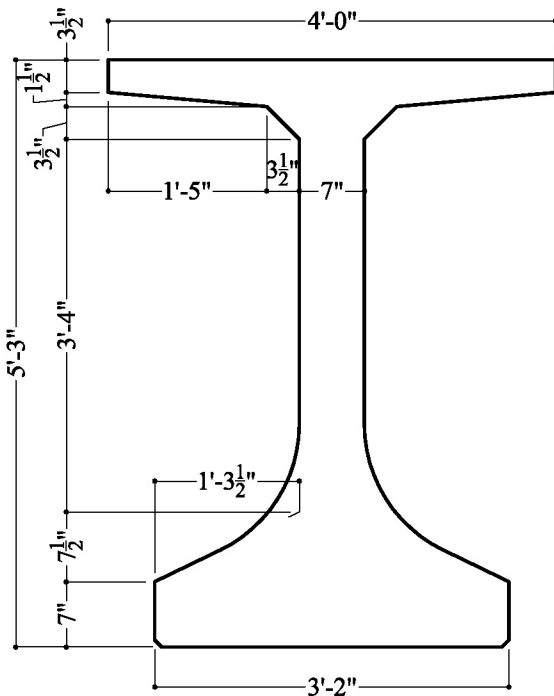
FIB 36

A=806.58 in² ;
Ix-x=127,544.64 in⁴
Iy-y=81,069.89 in⁴
Yb=16.49 in
Wt=840.19 plf



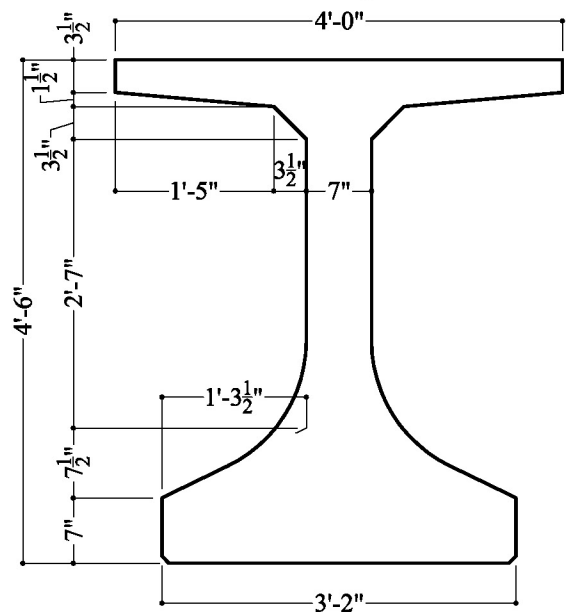
FIB 45

A=869.58 in²
Ix-x=226,580.72 in⁴
Iy-y=81,327.14 in⁴
Yb=20.21 in
Wt=905.81 plf



FIB 63

A=995.58 in²
Ix-x=530,313.25 in⁴
Iy-y=81,841.64 in⁴
Yb=27.96 in
Wt=1,037.06 plf



FIB 54

A=932.58 in²
Ix-x=359,929.12 in⁴
Iy-y=81,584.39 in⁴
Yb=24.04 in
Wt=971.44 plf

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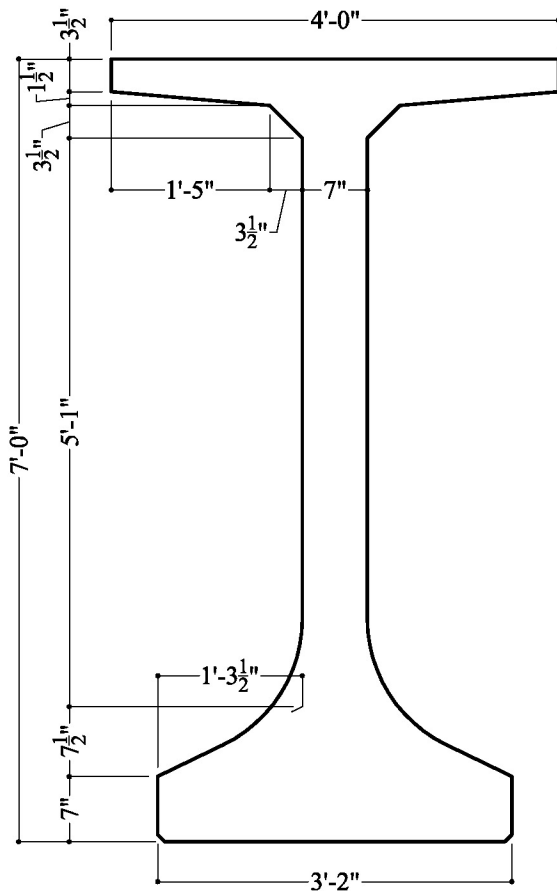
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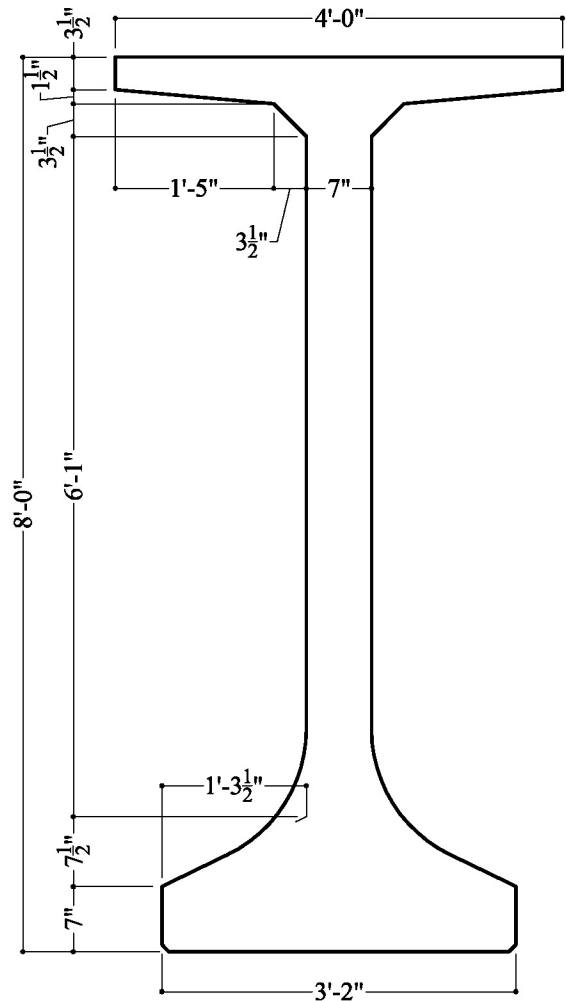


Standard
CONCRETE PRODUCTS



FIB 84

$A=1,142.58 \text{ in}^2$
 $I_x-x=1,187,000 \text{ in}^4$
 $I_y-y=82,442 \text{ in}^4$
 $Y_b=37.34 \text{ in}$
 $W_t=1,190.2 \text{ plf}$



FIB-96

$A=1,226.58 \text{ in}^2$
 $I_x-x=1,515,000 \text{ in}^4$
 $I_y-y=82,785 \text{ in}^4$
 $Y_b=42.82 \text{ in}$
 $W_t=1,277.7 \text{ plf}$

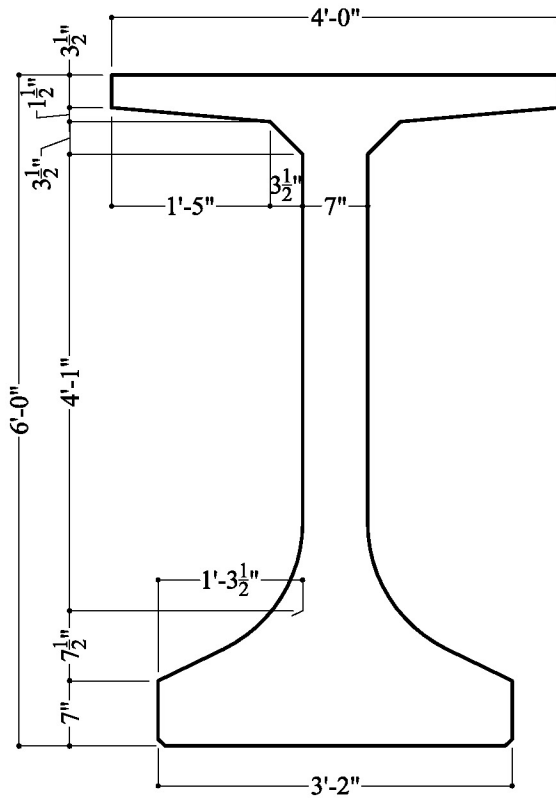
ALL WEIGHTS ARE NOMINAL.

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FIB-72

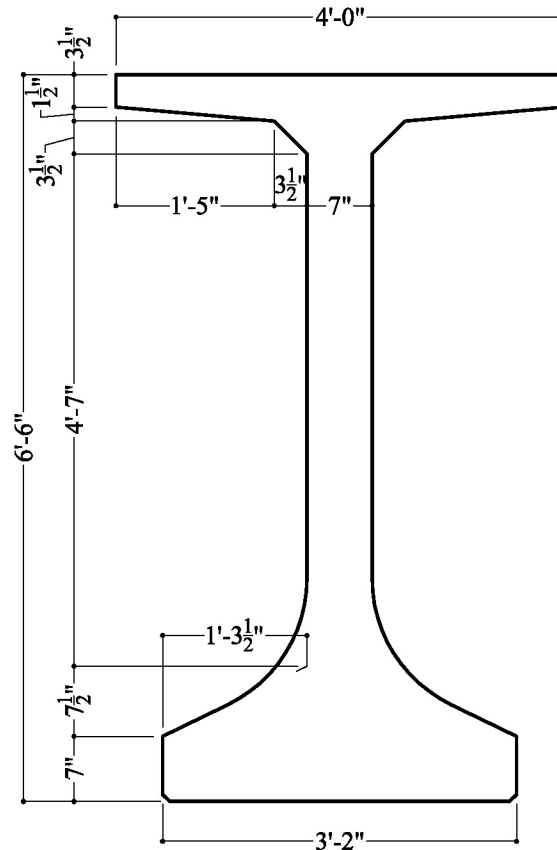
$$A=1,058.58 \text{ in}^2$$

$$I_x-x=740,415.59 \text{ in}^4$$

$$I_y-y=82,098.89 \text{ in}^4$$

$$Y_b=31.94 \text{ in}$$

$$W_t=1,102.68 \text{ plf}$$



FIB-78

$$A=1,100.58 \text{ in}^2$$

$$I_x-x=903,860.60 \text{ in}^4$$

$$I_y-y=82,270.39 \text{ in}^4$$

$$Y_b=34.63 \text{ in}$$

$$W_t=1,146.44 \text{ plf}$$

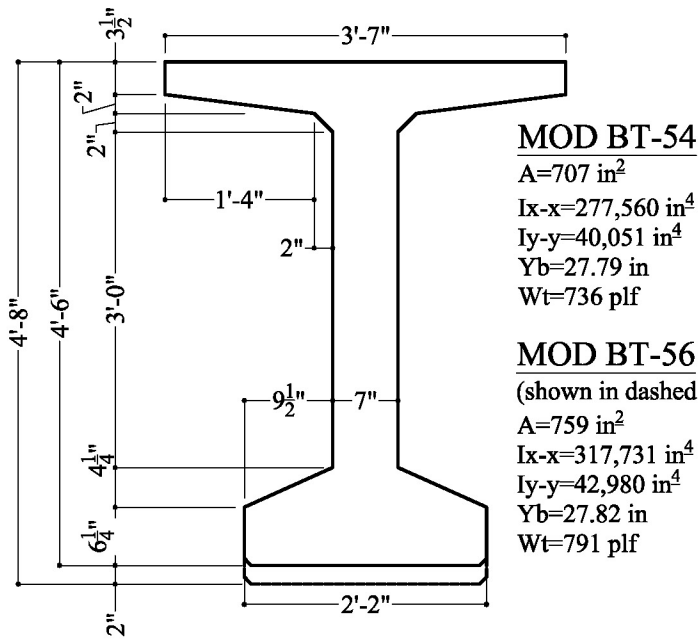
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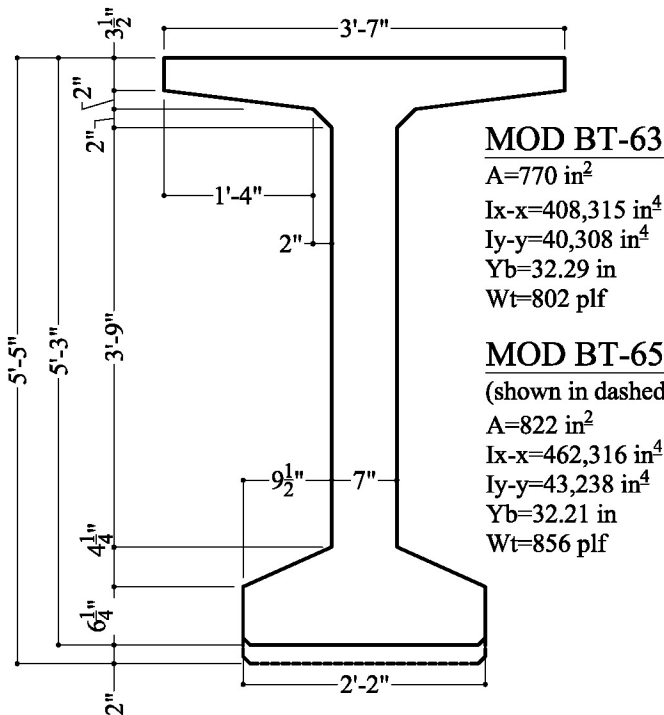
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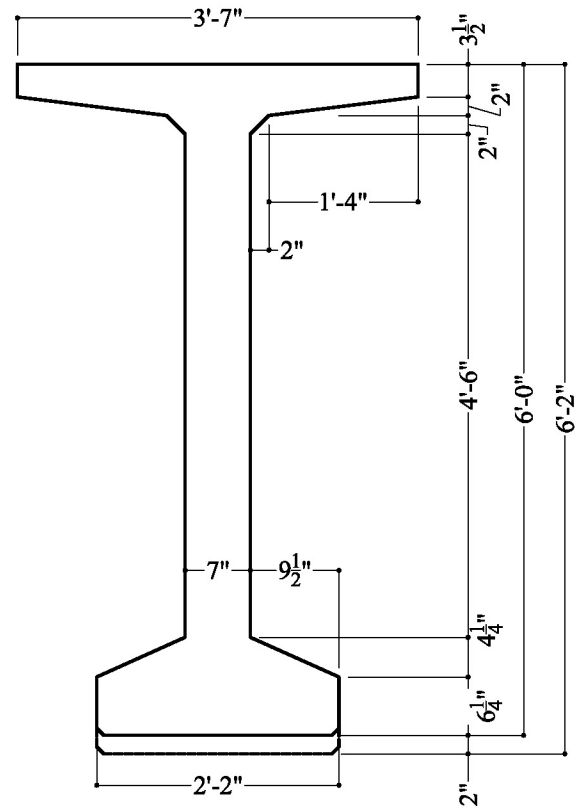
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MOD BT-56
 (shown in dashed line)
 $A=759 \text{ in}^2$
 $I_x=317,731 \text{ in}^4$
 $I_y=42,980 \text{ in}^4$
 $Y_b=27.82 \text{ in}$
 $W_t=791 \text{ plf}$



MOD BT-65
 (shown in dashed line)
 $A=822 \text{ in}^2$
 $I_x=462,316 \text{ in}^4$
 $I_y=43,238 \text{ in}^4$
 $Y_b=32.21 \text{ in}$
 $W_t=856 \text{ plf}$



MOD BT-72
 $A=833 \text{ in}^2$
 $I_x=570,260 \text{ in}^4$
 $I_y=40,566 \text{ in}^4$
 $Y_b=36.79 \text{ in}$
 $W_t=868 \text{ plf}$

MOD BT-74
 (shown in dashed line)
 $A=885 \text{ in}^2$
 $I_x=640,172 \text{ in}^4$
 $I_y=43,495 \text{ in}^4$
 $Y_b=36.57 \text{ in}$
 $W_t=922 \text{ plf}$

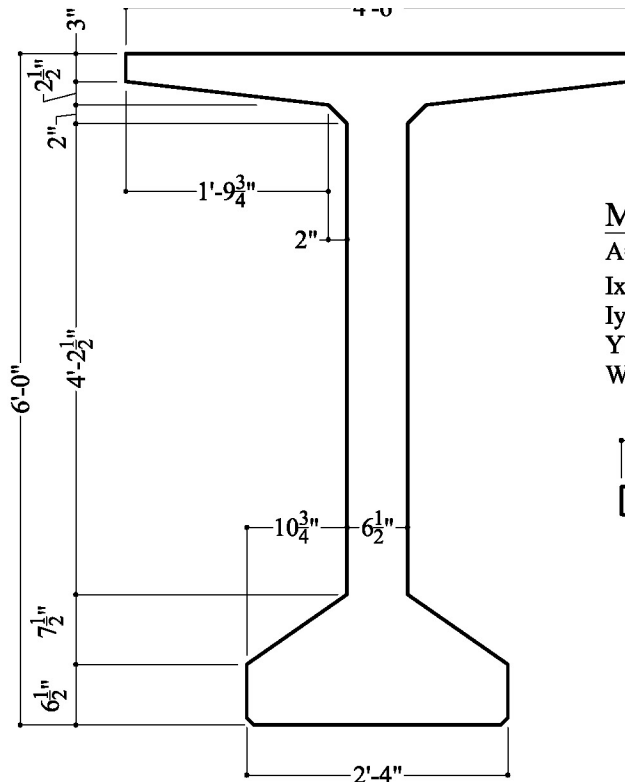
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MOD-FL- T-72

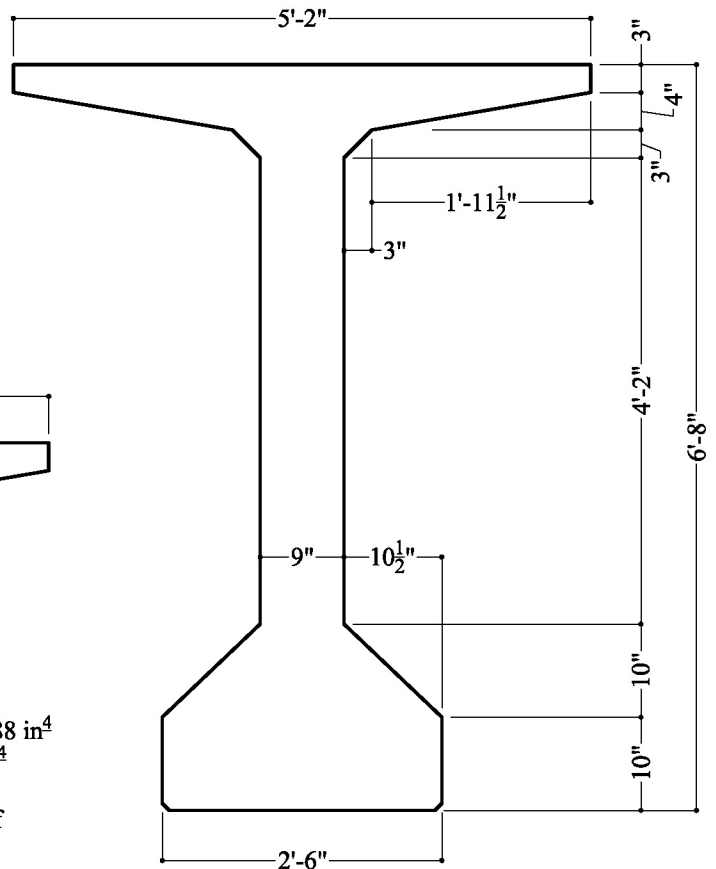
$A=898.7 \text{ in}^2$

$I_x-x=650,360.86 \text{ in}^4$

$I_y-y=67,034.35 \text{ in}^4$

$Y_b=35.59 \text{ in}$

$W_t=936.1 \text{ plf}$



MOD BT-80

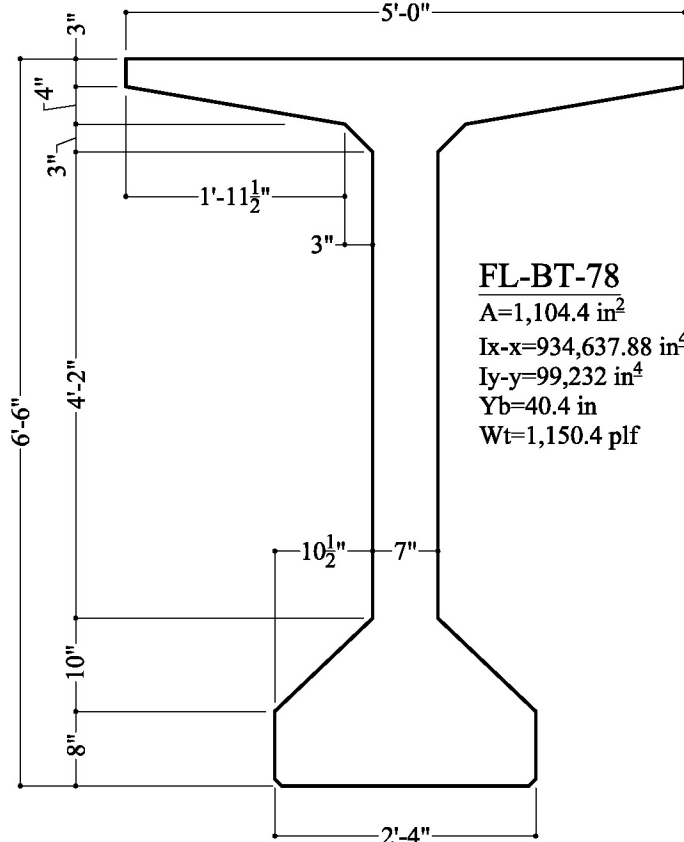
$A=1320.44 \text{ in}^2$

$I_x-x=1,111,302.17 \text{ in}^4$

$I_y-y=119,536.15 \text{ in}^4$

$Y_b=40.36 \text{ in}$

$W_t=1,375.5 \text{ plf}$



FL-BT-78

$A=1,104.4 \text{ in}^2$

$I_x-x=934,637.88 \text{ in}^4$

$I_y-y=99,232 \text{ in}^4$

$Y_b=40.4 \text{ in}$

$W_t=1,150.4 \text{ plf}$

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Technical drawing of a wide-flange beam cross-section. The drawing shows the following dimensions and labels:

- W**: Total width of the flange.
- tf**: Flange thickness.
- 1 $\frac{15}{16}$ "**: Distance from the outer edge of the flange to the centerline of the web.
- 4'-3 $\frac{1}{8}$ "**: Total depth of the beam.
- T**: Top flange.
- 8 $\frac{1}{2}$ "**: Distance from the outer edge of the flange to the centerline of the web.
- 1 $\frac{1}{2}$ "**: Distance from the outer edge of the flange to the centerline of the web.
- 1'-9"**: Depth of the web.
- dw**: Web thickness.
- 3"**: Distance from the centerline of the web to the outer edge of the flange.
- tw**: Web thickness.
- 12**: Distance from the centerline of the web to the outer edge of the flange.
- 3**: Distance from the centerline of the web to the outer edge of the flange.
- 10"**: Distance from the centerline of the web to the outer edge of the flange.
- bf**: Bottom flange.
- D**: Total depth of the beam.

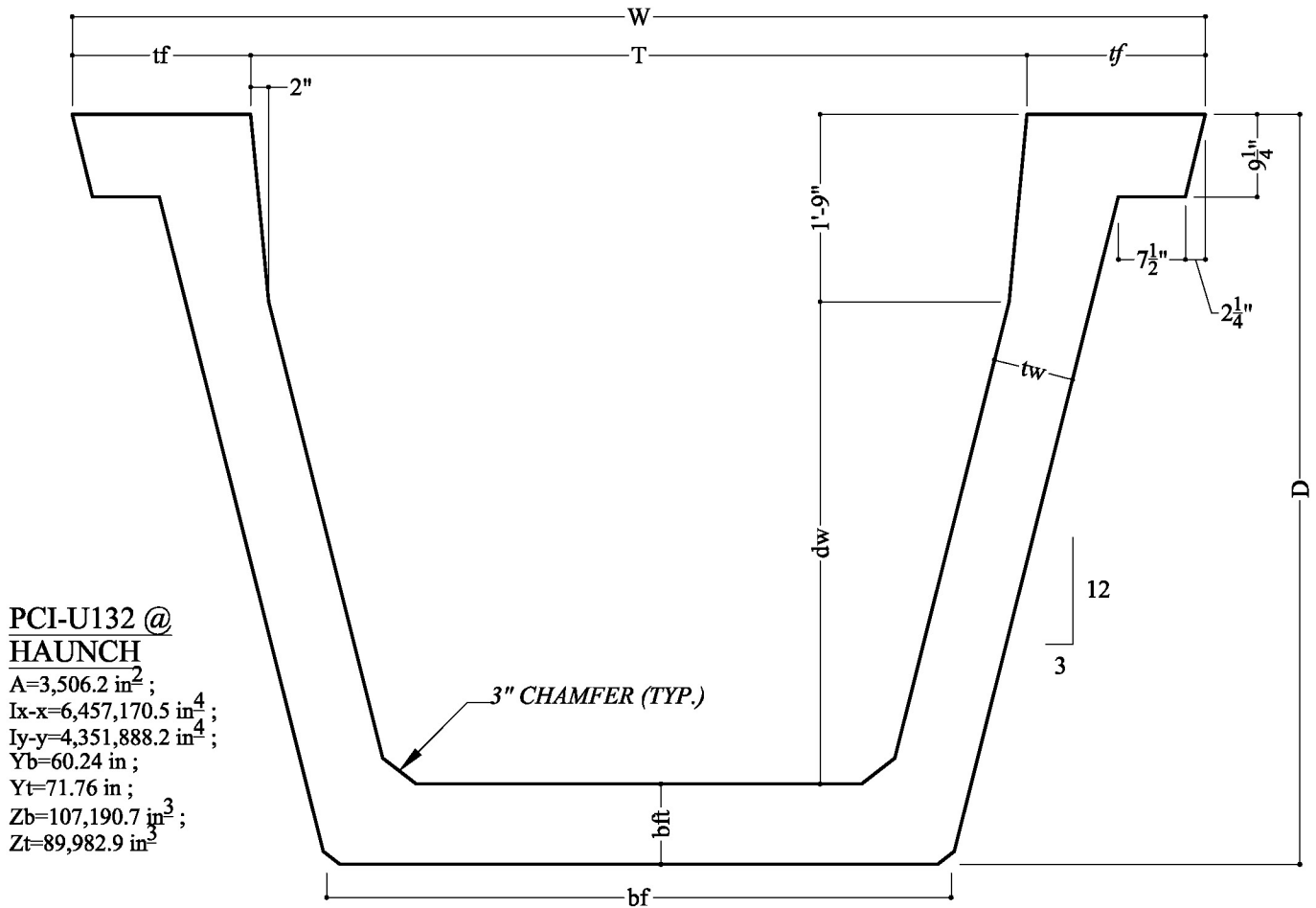
$A=1,478.3 \text{ in}^2$;
 $I_x-x=1,439,599.6 \text{ in}^4$;
 $I_y-y=931,164.7 \text{ in}^4$;
 $Y_b=29.94 \text{ in}$;
 $Y_t=42.06 \text{ in}$;
 $Z_b=48,082.8 \text{ in}^3$;
 $Z_t=34,227.3 \text{ in}^3$

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* CURVE GIRDER GEOMETRY									
GIRDER	D	dw	tw	W	T	tf	bf	bft	PLF
PCI-U72-3	6'-0"	3'-6"	9"	10'-1"	6'-9"	1'-8"	5'-10"	9"	2,117
PCI-U84-3	7'-0"	4'-6"	9"	10'-7"	7'-3"	1'-8"	5'-10"	9"	2,349
PCI-U96-3	8'-0"	5'-6"	9"	11'-1"	7'-9"	1'-8"	5'-10"	9"	2,581
PCI-U72-4	6'-0"	3'-6"	10"	10'-3"	6'-9"	1'-9"	6'-0"	9"	2,271
PCI-U84-4	7'-0"	4'-6"	10"	10'-9"	7'-3"	1'-9"	6'-0"	9"	2,529
PCI-U96-4	8'-0"	5'-6"	10"	11'-3"	7'-9"	1'-9"	6'-0"	9"	2,787
PCI-U84/132 (HAUNCH)	7'-0" - 11'-0"	4'-6" - 7'-6"	10"	-	-	-	-	18"	**303 KIPS

* Min. CURVATURE = 750' RADIUS
SPAN RANGE IS 175' to 300'

** TOTAL WEIGHT OF 98' LONG HAUNCHED PIER GIRDER



PCI-U132 @ HAUNCH

A=3,506.2 in²;
Ix-x=6,457,170.5 in⁴;
Iy-y=4,351,888.2 in⁴;
Yb=60.24 in;
Yt=71.76 in;
Zb=107,190.7 in³;
Zt=89,982.9 in³

PCI-U72-3

A=2,035 in²;
Ix-x=1,218,604.6 in⁴;
Iy-y=2,786,354.3 in⁴;
Yb=31.58 in;
Yt=40.42 in;
Zb=38,587.9 in³;
Zt=30,148.6 in³

PCI-U84-3

A=2,258 in²;
Ix-x=1,832,760.4 in⁴;
Iy-y=3,408,350.3 in⁴;
Yb=37.27 in;
Yt=46.73 in;
Zb=49,175.2 in³;
Zt=39,220.2 in³

PCI-U96-3

A=2,481 in²;
Ix-x=2,609,144.1 in⁴;
Iy-y=4,102,902.7 in⁴;
Yb=43.01 in;
Yt=52.99 in;
Zb=60,663.7 in³;
Zt=49,238.4 in³

PCI-U72-4

A=2,179 in²;
Ix-x=1,283,443.2 in⁴;
Iy-y=3,091,251.2 in⁴;
Yb=31.87 in;
Yt=40.13 in;
Zb=40,271.2 in³;
Zt=31,982.1 in³

PCI-U84-4

A=2,426 in²;
Ix-x=1,935,049.2 in⁴;
Iy-y=3,786,792.1 in⁴;
Yb=37.59 in;
Yt=46.41 in;
Zb=51,477.8 in³;
Zt=41,694.7 in³

PCI-U96-4

A=2,673 in²;
Ix-x=2,761,036.0 in⁴;
Iy-y=4,563,031.3 in⁴;
Yb=43.37 in;
Yt=52.63 in;
Zb=63,662.3 in³;
Zt=52,461.3 in³

ALL WEIGHTS ARE NOMINAL.

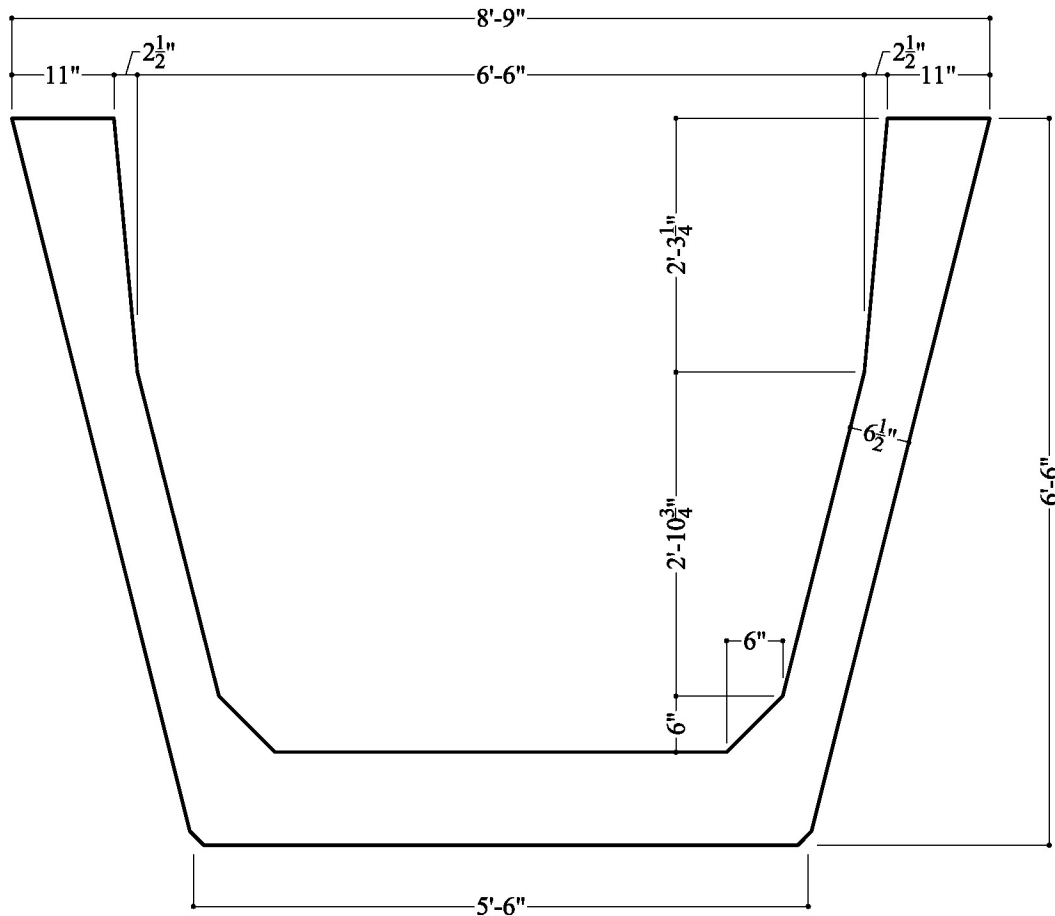
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Specialize Beam for light-rail automated people
mover system Miami, FL



U - 78" Beam

$A=1,738.2 \text{ in}^2$;
 $I_x-x=1,150,638.76 \text{ in}^4$;
 $I_y-y=2,025,713.3 \text{ in}^4$;
 $Y_b=29.89 \text{ in}$;
 $Y_t=48.11 \text{ in}$;
 $Z_b=38,495.77 \text{ in}^3$;
 $Z_t=23,916.83 \text{ in}^3$;
 $W_t=1810.63 \text{ plf}$

ALL WEIGHTS ARE NOMINAL.

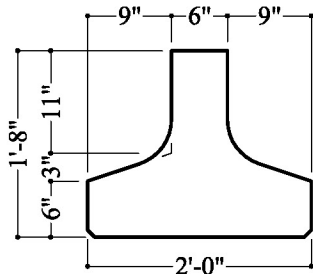
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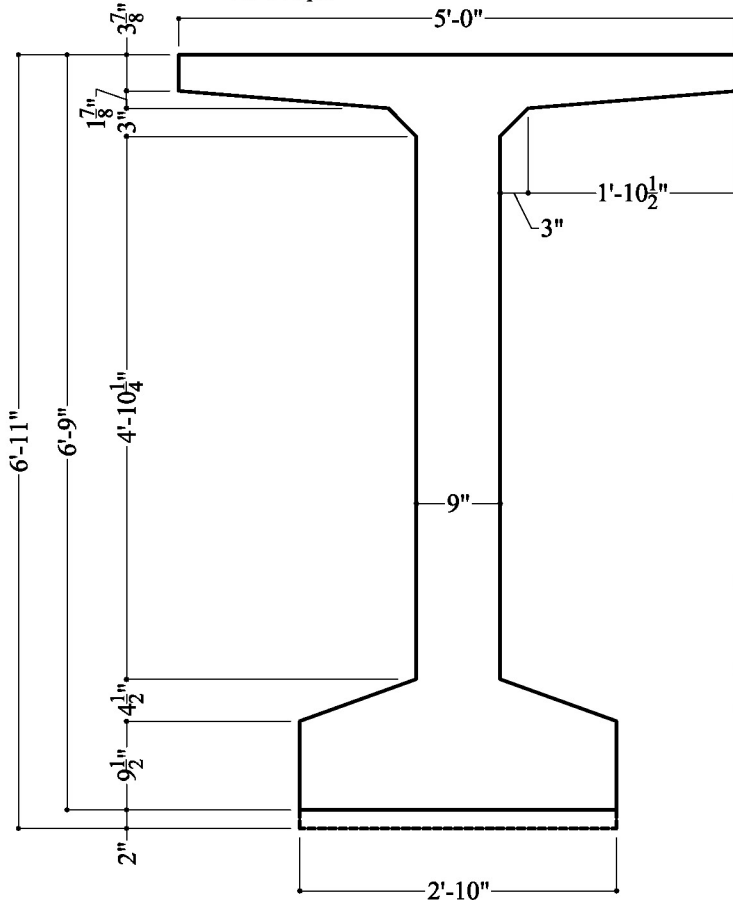
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Miscellaneous Beam Types



INVERTED - T

$A=259 \text{ in}^2$
 $I_x-x=8,248.75 \text{ in}^4$
 $I_y-y=7,141.59 \text{ in}^4$
 $Y_b=6.78 \text{ in}$
 $W_t=370 \text{ plf}$

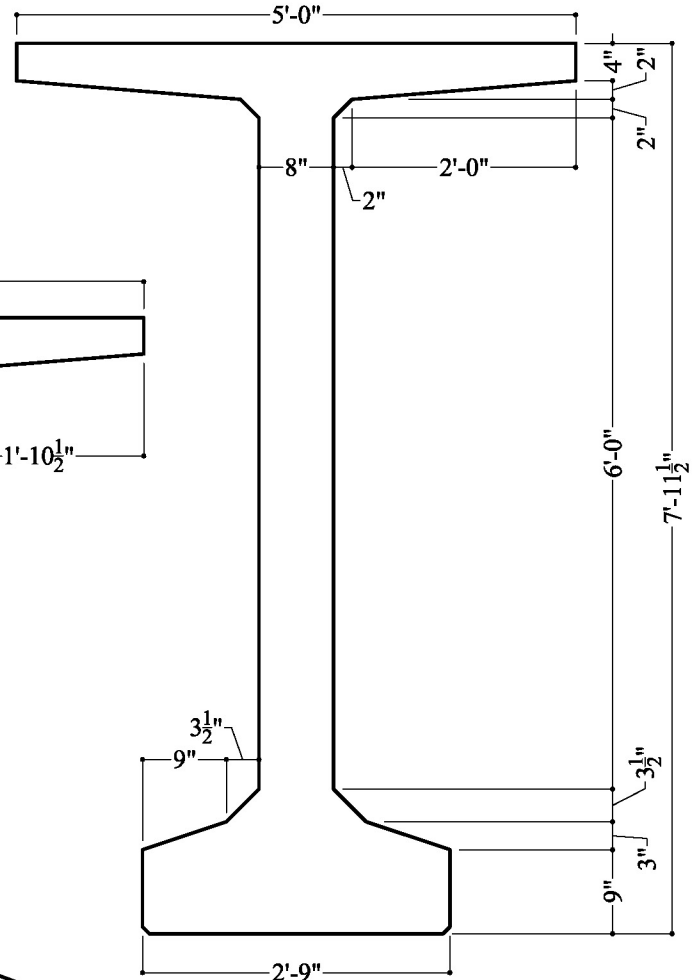


MOD BT-81

$A=1,283 \text{ in}^2$
 $I_x-x=1,126,248 \text{ in}^4$
 $I_y-y=121,056 \text{ in}^4$
 $Y_b=40.26 \text{ in}$
 $W_t=1,336 \text{ plf}$

MOD BT-83

(shown in dashed line)
 $A=1,351 \text{ in}^2$
 $I_x-x=1,236,217 \text{ in}^4$
 $I_y-y=127,607 \text{ in}^4$
 $Y_b=40.19 \text{ in}$
 $W_t=1,407 \text{ plf}$



PCEF-BT-95.5

$A=1,317 \text{ in}^2$
 $I_x-x=1,630,183 \text{ in}^4$
 $I_y-y=117,708 \text{ in}^4$
 $Y_b=47.87 \text{ in}$
 $W_t=1,372 \text{ plf}$

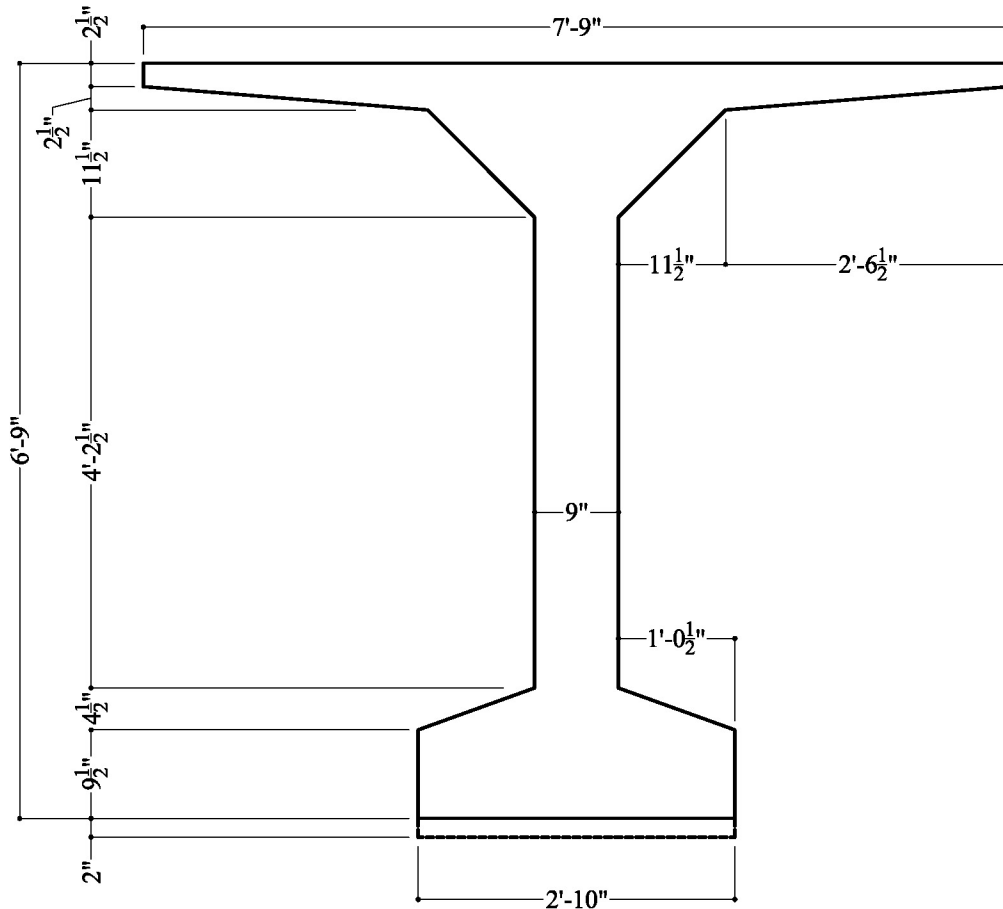
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ATLANTA AIRPORT GIRDERS

MOD BT-81

A=1,499 in²
 I_{x-x}=1,358,327.2 in⁴
 I_{y-y}=280,574.2 in⁴
 Y_b=45.32 in
 W_t=1,561plf

MOD BT-83

A=1,567 in²
 I_{x-x}=1,497,928.7 in⁴
 I_{y-y}=287,124.8 in⁴
 Y_b=45.31 in
 W_t=1,632plf

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